

BIOKINEMATIC MODEL OF IMPACT IN THE SPORTS

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In my abstract I indicated the reasons which have led me to build a biokinematic model of impact that can be used in the study of the **sports** movements in order to give the coach a valid help for the research of the most efficient **technique**, and to give to orthopedic more opportunities to identify the trauma causes.

Now we have to verify how the concepts of impact can be transferred, practically, into the movements in sports.

Therefore I would like to present the general **biokinematic** model of impact and I start by considering an athlete who clashes against the ground by his lower limbs and whose motion occurs along the axes Z, before and after the impact. The system is formed in the following manner:

- 1) by the athlete's mass m_1 which is placed above the concerned joint;
- 2) by the shock absorber K_1 , represented by the mass of the anatomic segment, standing under the concerned joint;
- 3) by the ground mass m_2 that we suppose to be concentrated;
- 4) by the shock absorber K_2 represented by the ground elasticity and then it depends on its nature (athletic ground, **tennis** court, boxing gloves and others);
- 5) by the fictitious shock absorber which acts in connection with the athlete's **g.c.** and indicates the moment of return and balance of the athlete, who rolls off an angle q_3 compared to his initial position of impact with the ground. In a few words, K_3 takes in to account the action of removal, exerted by the weight of the mass m_1 (the athlete).

The system is showed in fig. 1.

I'm going to provide an example to apply to the biokinematic model of impact. According to my intention, I consider an athlete who performs some jumps downwards from a determined height with following rebounds upwards (pliommetrical performance).

For the use of the **biokinematic** model of impact, I focus my attention on the impact which occurs between the athlete and the ground at the end of the descending way.

As coordinates of Lagrange, I choose the displacements q_1 and q_2 in the plane XZ related m_1 and m_2 during the time Dt , and the rotation q_3 of the athlete round the Y axe, normal to the plane XZ, and be O the point of intersection between the Y axe and the plane XZ.

I also specify that the concerned joint is the coxo-femoral and the axes X, Y, Z, represent respectively the transversal, sagittal and longitudinal axe.

The motion is defined by the **knowledge** of the **three** above-stated parameters, provided we except the case stated, for the execution of the model, so that:

- 1) the system is defined as plane, that's supposing that the movement takes place without considering the motion along the Y axe.
- 2) It's supposed that the point O is bound to move along the axe Z going through the two springs K_1 and K_2 that have been stated, and the equations of the motion of the two masses m_1 and m_2 are the following:

$$\begin{aligned} [1] \quad & a) q_1 \quad m_1 + S m_3 \cos q_3 - S m_3 q_2 \operatorname{sen} q_3 = -(q_1 - q_2) K_1 - (q_1 + R \cos q_3 \operatorname{tg} q_3) K_3; \\ & b) q_1 \cos q_3 S m_3 + q_3 \operatorname{Im} = - (q_1 + R \cos q_3 \operatorname{tg} q_3) K R \cos q_3; \\ & c) q_2 \quad m_2 = (q_1 - q_3) K_1 - q_2 K_2; \end{aligned}$$

with R which represents the **g.c.** distance of m_1 from the sagittal axe going through O , r which represents the distance of dm from the sagittal axe, so it's stated:

$$[2] \quad S_m = \int m_1 r \, dm \quad I_m = \int m_1 r^2 \, dm$$

In **a)** the term $S_m q_3 \sin q_3$ represents the centripetal force that must be considered unimportant compared to the other terms, and besides **it can be stated** that $\cos q_3 \cong 1$ and $\tan q_3 \cong q_3$, since the angles q_3 assume low values.

Thus the equations a), b), c), can be rewritten as follows:

$$[3] \quad \begin{aligned} q_1 m_1 + q_3 S_m + q_1 (K_1 + K_3) - q_2 K_1 + q_3 R K_3 &= 0 \\ q_1 S_m + q_3 I_m + q_1 R K_3 + q_3 R_2 K_3 &= 0 \\ q_2 m_2 - q_1 K_1 + q_2 (K_1 + K_2) &= 0 \end{aligned}$$

supposing that:

$$[4] \quad \begin{aligned} a &= \frac{I_m}{m_1 I_m - S_m^2} & b &= \frac{-S_m S_m}{m_1 I_m - S_m^2} & c &= \frac{m_1}{m_1 I_m - S_m^2} \end{aligned}$$

$$A_1 = -a(K_1 + K_3) + b R K_3; \quad A_2 = a K_1; \quad A_3 = a R K_3 + b R_2 K_3;$$

$$\begin{aligned} B_1 &= \frac{K_1}{m_2} & B_2 &= \frac{(K_1 + K_2)}{m_2} \\ C_1 &= b(K_1 + K_3) + c R K_3; & C_2 &= b K_1; & C_3 &= b R K_3 + c R_2 K_3 \end{aligned}$$

the [3] become:

$$[5] \quad \begin{aligned} q_1 &= A_1 q_1 + A_2 q_2 + A_3 q_3 \\ q_2 &= B_1 q_1 + B_2 q_2 \\ q_3 &= C_1 q_1 + C_2 q_2 + C_3 q_3 \end{aligned}$$

if we use a class of particular solutions like for the integrations:

$$[6] \quad q_j = H(j) e^{ht}$$

we obtain:

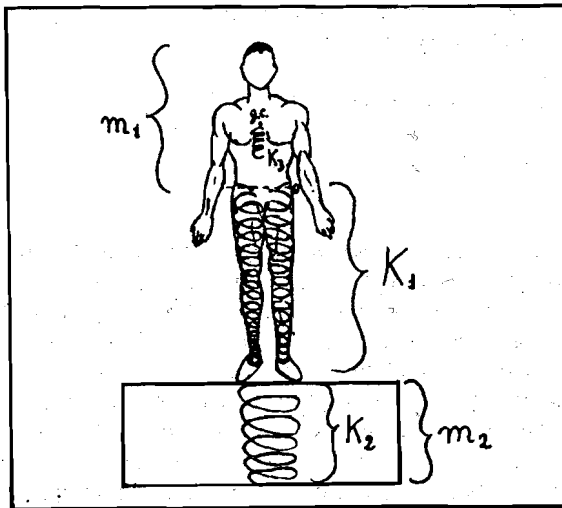
$$[7] \quad \begin{aligned} q_1 &= H_1(1) e^{h_1 t} + H_2(1) e^{\lambda_2 t} + \dots + H_6(1) e^{\lambda_6 t} \\ q_2 &= H_1(2) e^{h_1 t} + H_2(2) e^{\lambda_2 t} + \dots + H_6(2) e^{\lambda_6 t} \\ q_3 &= H_1(3) e^{h_1 t} + H_2(3) e^{\lambda_2 t} + \dots + H_6(3) e^{\lambda_6 t} \end{aligned}$$

with $h_1 \dots h_6$ roots of the equation belonging to the system [5].

By replacing [6] with [5] for $h = h_i$ the following relations are found among the H_i

$$[8] \quad \begin{aligned} H_i(2) &= \frac{B_1}{B_2 - \lambda_i^2} H_i(1) \\ H_i(3) &= \frac{H_i(1)}{A_3} \left[\frac{A_2 B_1}{B_2 - h_i^2} \cdot (A_1 - \lambda_i^2) \right] \end{aligned}$$

so the constants H which must be defined with the beginning conditions in the system [7] are six.



Biokinematic model of impact in the sport

For $t = 0$ it has to be: $q_1 = 0; q_2 = 0; q_3 = 0$
 $q_1 = V; q_2 = 0; q_3 = 0$

represents the athlete's speed at the moment of the impact.

If we wanted to examine the impact effect between the athlete and the ground on the knee of a triple jumper, we'd make some preliminary considerations.

The impact can provoke some traumas along the sagittal, transversal and longitudinal axe.

Therefore, for the examination of the impact on the **knee**, it is convenient to consider separately the motion along every axe with the opportune variants on the biomechanic model.

The studies made by Harmut **Krahl** and **KarlPeter** Knebel. Heiderlberg. West Germany published by Track Technique, emphasize the problem of the impact for high jumpers using the flop technique, being filmed at 300 photograms per second.

In fact, during the impact we can notice:

1) **a** remarkable rotation of the foot round the longitudinal axis when the heel touches the ground.

2) **While** resting the foot on the ground there is a great compression and a pronation of the heel as well as the bending of the plantar arch in the highest point of the tibiatarsal joint.

3) **A** position of complete pronation when all the foot plant is in contact with the ground.

From everything stated so far, it seem clear that the development of the most efficient technique for an athlete must take into account **his/her** anthropometric features as well as the shockabsorbing capabilities of the sporting facilities. Besides, the shoes must consider the approaching and removing speeds during, the clash, and also the relative positions taken

by the single anatomic segments during the movement, and finally the freedom degree or degrees of the articulations concerned.